## Thermogravimetric Study of the *Ln*<sub>2</sub>O<sub>3</sub>-Co-Co<sub>2</sub>O<sub>3</sub> System

III. Ln = Pr, Sm, Eu, and Tb

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Phase equilibria in the system  $Ln_2O_3$ -Co-Co<sub>2</sub>O<sub>3</sub> (Ln = Pr, Sm, Eu, and Tb) at 1200°C were studied at oxygen partial pressure ranging from 1 to  $10^{-12}$  atm O<sub>2</sub>. "Pr<sub>2</sub>CoO<sub>4</sub>," PrCoO<sub>3</sub>, and Pr<sub>4</sub>Co<sub>3</sub>O<sub>10</sub> are stable ternary compounds in the Pr<sub>2</sub>O<sub>3</sub>-Co-Co<sub>2</sub>O<sub>3</sub> system, while only LnCoO<sub>3</sub>-type compound is stable in the other systems. The standard Gibbs energies ( $\Delta G^{\circ}$ ) of reactions appearing in the systems were also determined from the oxygen partial pressures in equilibrium with three solid phases.  $\Delta G^{\circ}$  values for a reaction  $\frac{1}{2}Ln_2O_3 + CoO + \frac{1}{4}O_2 = Ln$ CoO<sub>3</sub> fit well with the linear  $\Delta G^{\circ}$  vs ionic radius relation reported previously. © 1988 Academic Press, Inc.

In the previous studies  $(1, 2) Ln_2O_3$ -Co-Co<sub>2</sub>O<sub>3</sub> (Ln = La, Nd, and Gd) was studied at 1200°C at oxygen partial pressures ranging from 1 to  $10^{-12}$  atm O<sub>2</sub>. In those systems, La<sub>2</sub>CoO<sub>4</sub>, La<sub>4</sub>Co<sub>3</sub>O<sub>10</sub>, LaCoO<sub>3</sub>, Nd<sub>4</sub> Co<sub>3</sub>O<sub>10</sub>, NdCoO<sub>3</sub>, and GdCoO<sub>3</sub> were stable ternary compounds, and those systems were classified into three types based upon the stable ternary compounds (2). Also the Gibbs energies of reactions which appear in the systems were determined, and the relationship between Gibbs energies for a common reaction,  $\frac{1}{2}Ln_2O_3 + CoO + \frac{1}{4}O_2 =$  $LnCoO_3$ , and the ionic radius of lanthanoid with 12 coordination was linear (2).

In this paper  $Pr_2O_3$ ,  $Sm_2O_3$ ,  $Eu_2O_3$ , and  $Tb_2O_3$  are chosen as  $Ln_2O_3$ .

 $MCoO_3$  (M = La-Ho, Y) was prepared by adding Na<sub>2</sub>CO<sub>3</sub> to solutions containing  $M(NO_3)_3$  and Co-nitrate to coprecipitate the oxides and then by calcining the oxides at 700°C (3). LaCoO<sub>3</sub> is hexagonal whereas the other  $MCoO_3$  compounds are or-0022-4596/88 \$3.00 366

thorhombic.  $Ln_2CoO_4$  and  $LnCoO_3$  (Ln = La-Sm, Gd, Dy, Er, Yb) were prepared in a high-temperature imaging furnace (4). The oxygen pressure range which can be used with this technique ( $8 \times 10^{-6}-200$  atm) makes it possible to attain the II and III oxidation states of Co. Demazeau *et al.* (5) reported that  $TCOO_3$  (T = Y, La-Lu) had been prepared under high oxygen pressure. LaCoO<sub>3</sub> is trigonal and NdCoO<sub>3</sub> is pseudotetragonal with orthorhombic symmetry and GdFeO<sub>3</sub>-type structure as found in the following  $TCoO_3$  phases.

 $Sm_2CoO_4$  was prepared at a high temperature of 2000°C with a mixture of  $Sm_2O_3/$ CoO = 1 mole ratio under oxygen atmosphere, and lattice constants were measured with a single crystal (6).  $Pr_2CoO_4$ was prepared under an atmosphere of N<sub>2</sub> in a temperature interval from 700 to 1200°C and its lattice constants were determined (7).

The compound Pr<sub>4</sub>Co<sub>3</sub>O<sub>10</sub>, with tetrago-

Copyright © 1988 by Academic Press, Inc. All rights of reproduction in any form reserved. nal structure and lattice constants  $a = 5.39 \pm 0.05$ ,  $c = 27.36 \pm 0.04$  Å, was prepared at 1100°C under partial pressure of  $10^{-4}$  atm by Cherepanov *et al.* (8). Electromotive force (emf) measurement was used to determine thermodynamic characteristics.

Kropanov *et al.* (9) reported on the temperature dependence of the dissociation pressure of  $LnCoO_3$  (Ln = Sm-Ho) into  $Ln_2O_3$ , CoO and  $O_2$  at 800–1200°C by emf measurement. The Ln-Co-O phase diagrams were roughly constructed at 1273°K. The only ternary compound formed under the conditions of the study is  $LnCoO_3$  with perovskite structure.

As summarized above, many researchers seem to be interested in compounds and very little work regarding phase equilibria has been performed.

The objectives of the present study were (1) to establish the detailed phase equilibria in these systems at 1200°C as a function of the oxygen partial pressure; (2) to calculate the thermochemical properties based upon the phase equilibria; (3) to ascertain in the Ln-Co-O system whether the phase diagram pattern would change with different lanthanoid elements; and (4) to determine whether a linear relationship between the Gibbs energy of reaction and lanthanoid ionic radius exists and is similar to that observed in the Ln-Fe-O (10) and Ln-V-O (11) systems.

#### **Experimental**

Analytical-grade  $Pr_6O_{11}$  (99.9%),  $Sm_2O_3$ (99.9%),  $Eu_2O_3$  (99.9%),  $Tb_4O_7$  (99.9%), and CoO (99.9%) were used as starting materials. Recently, the oxygen partial pressure ranges in which  $Pr_2O_3$  and  $Tb_2O_3$  are stable were determined at 1000, 1100, and 1200°C (12). According to the results,  $Pr_6O_{11}$  and  $Tb_4O_7$  are stable in the oxygen partial pressure higher than  $10^{-0.70}$  and  $10^{-1.75}$ , respectively.  $Pr_6O_{11}$  and  $Tb_4O_7$  were reduced to  $Pr_2O_3$  and  $Tb_2O_3$  at 1200°C in the

oxygen partial pressure of  $10^{-10}$  atm for 5 hr (11). Hexagonal, light green  $Pr_2O_3$  and white Tb<sub>2</sub>O<sub>3</sub> with C-form were confirmed by the powder X-ray diffraction method (13, 14) and the compositions were determined to be Pr<sub>2</sub>O<sub>3.00</sub> and Tb<sub>2</sub>O<sub>3.00</sub> by EDTA titration. Sm<sub>2</sub>O<sub>3</sub>, Eu<sub>2</sub>O<sub>3</sub>, and CoO were preliminarily dried at 1200°C in air. Mixtures with desired molar ratios of  $Ln_2O_3/CoO$ were obtained by mixing the calculated amounts of constituent binary oxides thoroughly in an agate mortar. The mixtures thus obtained were heated at 1200°C several times during the intermediate mixing and were treated by the same procedures as those described previously (15).

The apparatus and means for controlling the oxygen partial pressures and keeping a constant temperature, the method of thermogravimetry, and the criterion for the establishment of equilibrium are the same as those described previously (15, 16).

X-ray powder analysis, employing Ni-filtered  $CuK\alpha$  radiation from the compounds in the Pr-Co-O, Sm-Co-O, and Tb-Co-O systems, and Mn-filtered Fe  $K\alpha$  radiation for the compounds in the Eu-Co-O system, was used to characterize the phases present in the quenched samples. Lattice constants were also determined by the Xray powder method with a slow scanning speed of  $0.5^{\circ} 2\theta/\min$ . A standard specimen of external silicon was used as  $2\theta$  calibrant. Mixtures of CO<sub>2</sub> and H<sub>2</sub> or CO<sub>2</sub> and O<sub>2</sub> were used to obtain the required oxygen partial pressure. The actual oxygen partial pressures were measured by means of a soid electrolytic cell,  $(ZrO_2)_{0.85}(CaO)_{0.15}$  (17).

## **Results and Discussion**

#### (1) Phase Equilibria

 $Pr_2O_3$ -Co- $Co_2O_3$  system. Eight mixtures with  $Pr_2O_3$ /CoO mole ratios of 6/4, 5.5/4.5, 4.75/5.25, 4.4/5.6, 4/6, 3/5, 3/7, and 2/8 were prepared to use in thermogravimetry. In



FIG. 1. The relationships between  $-\log(P_{O_2}/\text{atm})$  and the weight change,  $W_{O_2}/W_T$ , of samples in the Pr system. (a)  $Pr_2O_3/CoO = 6/4$ , (b)  $Pr_2O_3/CoO = 4.4/5.6$ , (c)  $Pr_2O_3/CoO = 3/5$ , (d)  $Pr_2O_3/CoO = 3/7$ .

Fig. 1 the relationships between the oxygen partial pressure,  $-\log(P_{O_2}/\text{atm})$ , on the ordinate and the weight change,  $W_{O_2}/W_T$ , on the abscissa are shown for four representative samples, (a) 6/4, (b) 4.4/5.6, (c) 3/5, and

(d) 3/7.  $W_{O_2}$  is the weight increase of the samples relative to the reference weight at log  $P_{O_2} = -12.00$ , at which  $Pr_2O_3$  and Co-metal coexists, and  $W_T$  is the total weight gain from the reference weight to the

As shown in Fig. 1 abrupt weight changes take place at values of  $-\log P_{O_2}$  of 9.30, 5.73, 3.60, 3.10, 3.05, and 2.05. These values reflect the oxygen partial pressures at which three solid phases are in equilibrium. Among these values,  $\log P_{O_2} = -9.30$  corresponds to the oxygen partial pressure of a reaction, Co +  $\frac{1}{2}O_2 = CoO(1)$ .

The identification of phase was carried out on samples which were quenched at different conditions of the oxygen partial pressure. Part of the results are shown in Table I as the two-phase combinations.

Based upon the thermogravimetric results and the phase identification, the phase diagram was constructed with apices of  $Pr_2O_3$ , Co, and  $Co_2O_3$  as shown in Fig. 2. Numerical values in the three solid fields in Fig. 2 indicate the six equilibrium oxygen

partial pressures as  $-\log P_{O_2}$  described above. Dotted lines represent the isooxygen partial pressures of the two-phase fields and solid lines are phase boundaries. Seven phases, Pr<sub>2</sub>O<sub>3</sub>(R), Pr<sub>6</sub>O<sub>11</sub>, Co, "Pr<sub>2</sub>CoO<sub>4</sub>" (A),  $Pr_4Co_3O_{10}(B)$ ,  $PrCoO_3(C)$ , and CoO(D)are stable in the system. At 1200°C Pr<sub>2</sub>O<sub>3</sub> is stable in the oxygen partial pressure range lower than  $\log P_{O_2} = -0.74 \pm 0.05$ . Pr<sub>6</sub>O<sub>11</sub> is not shown in Fig. 2 to avoid confusion.  $Co_2O_3$  and  $Co_3O_4$  are not found.  $PrCoO_3$ , Pr<sub>4</sub>Co<sub>3</sub>O<sub>10</sub>, and "Pr<sub>2</sub>CoO<sub>4</sub>" have nonstoichiometric compositions. "Pr<sub>2</sub>CoO<sub>4</sub>" does not mean stoichiometric Pr<sub>2</sub>CoO<sub>4</sub> which is indicated by an open circle, A, in Fig. 2. Here, the quotation marks represent the component of the phase as well as wüstite which is indicated by "FeO." The X-ray powder pattern of "Pr<sub>2</sub>CoO<sub>4</sub>" which was made at log  $P_{O_2} = -3.30$  and -5.00 is similar to that of Kniga et al. (7). They indexed the structure of Pr<sub>2</sub>CoO<sub>4</sub> as tetragonal but Flamand and Berjoan (4) indexed it as



FIG. 2. Phase equilibria in the  $Pr_2O_3$ - $Co-Co_2O_3$  system at 1200°C. Numerical values in three- and two-phase regions are the oxygen partial pressures in  $-\log(P_{O_2}/\text{atm})$  in equilibrium. Symbols are the same as those in Table III.

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Composition (mole%)		$-\log P_{O_2}$	Time (hr)		
		(atm)		Phase	
Pr <sub>2</sub> O <sub>3</sub>	CoO				
		10.00	-	<b>D</b> O	
00	40	10.00	17	$Pr_2O_3$	$+ C_{0}$
		9.00 5.00	20	$Pr_2O_3$	+ 000
		3.00	20	$P_2O_3$	+ $P_1^2 C O O_4$
		2.50	20	$PT_2O_3$	+ $Pr_4Co_3O_{10}$
		1.50	24	$PT_2O_3$	+ $PrCoO_3$
44	56	0.00	20	$PI_6 U_{11}^{*}$	$+ PrcoO_3$
44	20	2.00	20 12	$PF_2COU_4$	+ CoO
37 5	67 5	3.30	23		+ $PI_4CO_3O_{10}$ + $Pr Co O$
57.5	02.5	3.30	25	DrCaO	+ $P_{14}CO_{3}O_{10}$
20	80	2.30	20		$+ PI_4 CO_3 O_{10}$
20	00	2.50	20	CoO	+ $PrC_{2}COO_{4}$
		2.50	20	C00	+ PrCoO <sub>3</sub>
		0.00	0	000	+ FIC00 <sub>3</sub>
Eu <sub>2</sub> O <sub>3</sub>	CoO				
60	40	10.00	6	Eu <sub>2</sub> O <sub>3</sub>	+ Co
		9.00	8	$Eu_2O_3$	+ CoO
		2.00	20	$Eu_2O_3$	+ CoO
		0.68	43	Eu <sub>2</sub> O <sub>3</sub>	+ EuCoO <sub>3</sub>
40	60	2.00	20	$Eu_2O_3$	+ CoO
		0.68	43	EuCoO <sub>3</sub>	+ CoO
20	80	2.00	20	EuCoO <sub>3</sub>	+ CoO
Sm <sub>2</sub> O <sub>3</sub>	CoO				
63	37	10.00	14	Sm <sub>2</sub> O <sub>3</sub>	+ Co
		9.00	14.5	$Sm_2O_3$	+ CoO
		0.68	8	Sm <sub>2</sub> O <sub>1</sub>	+ SmCoO <sub>3</sub>
30	70	10.00	14	Sm <sub>2</sub> O <sub>3</sub>	+ Co
		9.00	14.5	$Sm_2O_3$	+ CoO
		0.68	8	SmCoO <sub>3</sub>	+ CoO
Tb <sub>2</sub> O <sub>3</sub>	CoO				
60	40	10.00	8	Tb <sub>2</sub> O <sub>3</sub>	+ Co
		9.00	8	Tb <sub>2</sub> O <sub>3</sub>	+ CoO
		2.00	15	Tb <sub>2</sub> O <sub>3</sub>	+ CoO
		0.68	44	Tb <sub>2</sub> O <sub>3</sub>	+ CoO
		0	14	Tb <sub>4</sub> O <sub>7</sub>	+ TbCoO <sub>3</sub>
25	75	10.00	8	Tb <sub>2</sub> O <sub>3</sub>	+ Co
		9.00	8	Tb <sub>2</sub> O <sub>3</sub>	+ CoO
		0.68	44	Tb <sub>2</sub> O <sub>3</sub>	+ CoO
		0	14	TbCoO <sub>3</sub>	+ CoO
				-	

TABLE I Identification of Phase

<sup>a</sup> This phase is not represented in Fig. 2.

Compound	$-\log P_{O_2}$ (atm)	Other phases	a (Å)	<i>b</i> (Å)	c (Å)	V (Å <sup>3</sup> )	Ref.
Pr <sub>4</sub> Co <sub>3</sub> O <sub>10</sub>	3.30	"Pr2CoO4"	$5.376 \pm 0.002$	$5.458 \pm 0.002$	$27.34 \pm 0.02$	$802.3 \pm 0.7$	Present
	3.30	CoO	$5.377 \pm 0.002$ $5.390 \pm 0.005$	$5.459 \pm 0.002$	$27.34 \pm 0.02$ $27.36 \pm 0.04$	$802.7 \pm 0.6$	Present (8)
"Pr <sub>2</sub> CoO <sub>4</sub> "	3.30	Pr <sub>4</sub> Co <sub>3</sub> O <sub>10</sub>	$3.878 \pm 0.007$		$12.24 \pm 0.05$	$184.2 \pm 1.0$	Present
	3.30	Pr <sub>2</sub> O <sub>3</sub>	$3.881 \pm 0.008$		$12.27 \pm 0.06$	$184.8 \pm 1.2$	Present
			$3.87 \pm 0.01$		$12.65 \pm 0.02$		(7)
PrCoO3	1.50	CoO	$7.575 \pm 0.002$			$434.6 \pm 0.4$	Present
	1.50	$Pr_2O_3$	$7.572 \pm 0.003$			$434.2 \pm 0.4$	Present
			7.572				(19)
			$5.344 \pm 0.007$	$5.358 \pm 0.007$	$7.60 \pm 0.01$		(3)
			5.331	5.373	7.587	212.44	(20)
SmCoO <sub>3</sub>	0.68	CoO	$5.284 \pm 0.006$	$5.343 \pm 0.006$	$7.506 \pm 0.006$	$211.9 \pm 0.4$	Present
	0.68	$Sm_2O_3$	$5.283 \pm 0.005$	5.344 ± 0.005	$7.502 \pm 0.005$	$211.8 \pm 0.03$	Present
			$5.294 \pm 0.002$	$5.352 \pm 0.002$	$7.504 \pm 0.003$	$212.6 \pm 0.2$	(5)
TbCoO3	0	Tb <sub>4</sub> O <sub>7</sub>	$5.209 \pm 0.011$	$5.393 \pm 0.006$	$7.409 \pm 0.010$	$208.1 \pm 0.6$	Present
	0	CoO	$5.203 \pm 0.008$	$5.398 \pm 0.005$	$7.408 \pm 0.006$	$207.7 \pm 0.4$	Present
			$5.209 \pm 0.002$	$5.402 \pm 0.002$	$7.425 \pm 0.003$	$208.9 \pm 0.2$	(5)
EuCoO <sub>3</sub>	0.68	CoO	5.259 ± 0.001	$5.370 \pm 0.001$	$7.481 \pm 0.002$	$211.2 \pm 0.1$	Present
	0.68	Eu <sub>2</sub> O <sub>3</sub>	$5.258 \pm 0.001$	$5.371 \pm 0.001$	$7.479 \pm 0.002$	$211.2 \pm 0.1$	Present
			$5.261 \pm 0.002$	$5.369 \pm 0.002$	$7.488 \pm 0.003$	$211.5 \pm 0.2$	(5)

TABLE II LATTICE CONSTANTS OF THE COMPOUNDS

monoclinic. However, they did not mention the nonstoichiometry of  $Pr_2CoO_4$ .

The  $Pr_4Co_3O_{10}$  with tetragonal structure was prepared at 1100°C under partial O pressure of  $10^{-4}$  atm (8). At 1200°C the compound is stable in the oxygen partial pressure from  $10^{-3.60}$  to  $10^{-2.05}$  also.

The relationships between the composition and the oxygen partial pressure of the solid solutions are represented with linear equations,  $N_0/N_{PrCoO_3} = 0.0152 \log P_{O_2}$ -0.030 for the PrCoO\_3 solid solution,  $N_0/N_{Pr_4CO_3O_{10}} = 0.0907 \log P_{O_2} + 0.186$  for the Pr\_4CO\_3O\_{10} solid solution, and  $N_0/N_{Pr_2CoO_4} =$  $0.0342 \log P_{O_2} + 0.276$  for the Pr\_2CoO\_4 solid solution. Here, N denotes the mole fraction of the subscripts. Data for the linear equation concerning the CoO solid solution were reported earlier (1).

Lattice constants of the ternary compounds are listed in Table II. The assignment of the indices of  $Pr_4Co_3O_{10}$  were attempted with the aid of the orthorhombic data of  $La_4Co_3O_{10}$  although Cherepanov et al. (8) indexed them to be the tetragonal structure described above. The volume values seem to be large, but that of  $La_4Co_3O_{10}$ is  $\sim 800$  Å<sup>3</sup>, also. Judging from the values of  $Pr_4Co_3O_{10}$  in Table II, there is no effect by the coexisting phases. Values of  $Pr_4Co_3O_{10}$ which were quenched at log  $P_{0_2} = -2.50$ are almost the same as those quenched at  $\log P_{0_2} = -3.30$ . For Pr<sub>2</sub>CoO<sub>4</sub>, Kniga et al. (7) and Flamand and Berjoan (4) reported lattice constants with tetragonal and monoclinic systems, respectively. Based upon Kniga's assignment of index, the present values were determined. The errors are still large, but the values are comparable to those of Kniga et al. and coexisting phases do not affect the values of lattice constants. For lattice constants of PrCoO<sub>3</sub>, two different systems were adopted as shown in Table II. Here, the cubic system was used because its index data were available. Coexisting phases do not affect the values of lattice constants.

Three types of phase diagrams concerning the Ln-Co-O system were reported (2). According to the classification, the present one seems to belong to the A type, in which three ternary compounds,  $Ln_2$  $CoO_4$ ,  $Ln_4CoO_3O_{10}$ , and  $LnCoO_3$ , are stable. But the present type is different from the A type, that of  $La_2O_3-Co-Co_2O_3$ , because the present type has a two-phase field,  $Pr_2O_3 + CoO$ . Because of this twophase region, three-phase solid regions,  $Pr_2O_3 + CoO + "Pr_2CoO_4"$  and  $Pr_2O_3 + Pr_2O_3$ CoO + Co-metal, appear, which are not stable in the A type. Therefore, I would like to assign the present one to a new type, type D.

 $Ln_2O_3$ -Co-Co<sub>2</sub>O<sub>3</sub> (Ln = Sm, Eu, and Tb). In Fig. 3 the relationships between the oxygen partial pressure and the composition are presented for three mixtures represented by the following mole ratios of starting materials: (a)  $Sm_2O_3/CoO = 6.32/3.68$ , (b) 4/6, and (c) 3/7 for the Sm system; (a)  $Eu_2O_3/CoO = 6/4$ , (b) 4/6, and (c) 2/8 for the Eu system; and (a)  $Tb_2O_3/CoO = 6/4$ , (b) 4/6, (c) 2.5/7.5 for the Tb system. The reference weight was also set at log  $P_{O_2}$  = -12.00 at which two phases,  $Ln_2O_3 + Co_$ metal, are stable. These patterns are very simple. Abrupt weight changes take place at two oxygen partial pressures: one is the common value,  $\log P_{\Omega_2} = -9.30$ , at which the reaction,  $Co + \frac{1}{2}O_2 = CoO$ , appears and the others are  $1.82 \pm 0.05$  for the Sm system,  $1.42 \pm 0.03$  for the Eu system, and  $0.53 \pm 0.07$  for the Tb system.

The results of the phase identification of the three systems are tabulated in Table I together with those of the Pr system. The  $Sm_2O_3$ -Co-Co<sub>2</sub>O<sub>3</sub> system is drawn in Fig. 4 as the representative. The patterns of the other two systems are almost the same provided that the solid solution ranges of the  $LnCoO_3$  and the oxygen partial pressure in equilibrium with three solid phases,  $Ln_2O_3$ +  $LnCoO_3$  + CoO, are different as described above.

In Table III the composition of the compounds at representative points, its symbol, the stability of the compounds in log  $P_{O_2}$ , and the activities of the components in the solid solutions are tabulated together with those of the Pr system. From these data and Fig. 3, phase diagrams of the other two can be easily deduced by the reader. These phase diagrams belong to the C type (2) in which one ternary compound,  $LnCoO_3$ , is stable.

SmCoO<sub>3</sub> and EuCoO<sub>3</sub> have a small range of nonstoichiometry, which is represented by the equations  $N_{\rm O}/N_{\rm SmCoO_3} = 0.0110 \log P_{\rm O_2}$  and  $N_{\rm O}/N_{\rm EuCoO_3} = 0.0141 \log P_{\rm O_2}$ , while TbCoO<sub>3</sub> is stoichiometric.

## (2) The Standard Gibbs Energy of Reaction

On the basis of the established phase diagrams, the standard Gibbs energies of reac-

TABLE III

Compositions, Symbols, Stability Ranges in Oxygen Partial Pressures, and Activities in Solid Solutions

Component	Composition	Symbol	$-\log P_{O_2}$ (atm)	log a <sub>i</sub>	
РтСоО3	PrCoO <sub>2.92</sub>	<i>C</i> 1	3.05	0	
	PrCoO <sub>2.94</sub>	$C_2$	2.05	0.0344	
	PrCoO2.97	$C_3$	0.80	0.0668	
Pr4C03O10	Pr4C03O9.86	<b>B</b> 1	3.60	0	
	PT4C03O9.90	<b>B</b> <sub>2</sub>	3.10	0.0295	
	Pr4C03O9.91	B <sub>3</sub>	3.05	0.0318	
	Pr4C03O10.0	B <sub>4</sub>	2.05	0.0544	
PT2CoO4	PT2CoO4.08	$A_1$	5.73	0	
	Pr2CoO4.15	A2	3.60	-0.124	
	PT2CoO4.17	A3	3.10	-0.164	
SmCoO3	SmCoO <sub>2.98</sub>	$c_{i}$	1.80	0	
	SmCoO <sub>3.00</sub>	Cź	0	~0.0091	
EuCoO3	EuCoO <sub>2.98</sub>	Cï	1.42	0	
	EuCoO <sub>3.00</sub>	Cž	0	-0.0071	
TbCoO3	TbCoO <sub>3.00</sub>	$C_{1}'''$	0.53-0	0	
CoO	CoO <sub>0.991</sub>	$D_1$	9.30	0	
	CoO <sub>0.996</sub>	D <sub>2</sub>	5.73	0.0118	
	CoO <sub>0.998</sub>	$D_3$	3.60	0.0152	
	CoO <sub>0.999</sub>	$D_4$	3.05	0.0157	
	CoO1.000	$D_5$	1.82	0.0160	
	CoO1.001		1.42	0.0159	
	CoO <sub>1.002</sub>		0.53	0.0153	



FIG. 3. The relationships between  $-\log(P_{O_2}/atm)$  and the weight change,  $W_{O_2}/W_T$ , of samples in the Sm, Eu, and Tb systems. The compositions of the starting materials indicated by (a), (b), and (c) are described in the text.

tions, which are given in Table IV, were calculated by the equation,  $\Delta G^{\circ} = -RT \ln K$ . The activities in Table III and those of CoO in the CoO solid solution, obtained

from previous data (1), were used to calculate K values. By subtracting equation (1) from equation (2), one obtains an equation,  $\frac{1}{2}Pr_2O_3 + CoO + \frac{1}{4}O_2 = PrCoO_3$ , with  $\Delta G^{\circ}$ 



FIG. 4. Phase equilibria in the  $Sm_2O_3$ -Co-Co<sub>2</sub>O<sub>3</sub> system at 1200°C. Numerical values in the threephase regions are the oxygen partial pressures in - log( $P_{O_2}$ /atm) in equilibrium. Symbols are the same as those in Table III.

= -25.9 kJ. The standard Gibbs energy for the formation of PrCoO<sub>3</sub> from common oxides was refined by Petrov *et al.* (18) and an equation,  $\Delta G^{\circ} = -184,760 + 0.1063 \times 10^3$ T (J), was obtained. From this equation, the  $\Delta G^{\circ}$  value at 1200°C was calculated to be -28.2 kJ, which is in fairly good agreement with the present one. For reactions (1)  $\times 2$ and (2),  $\Delta G^{\circ} \pm 120 = -96,470 + 46.92 \text{ T}$  (K  $\leq 1473$ ) and  $\Delta G^{\circ} \pm 140 = -176,350 +$ 99.55 T (K  $\leq 1473$ ) were presented by Cherepanov *et al.* (8) using emf measurements, respectively. At 1200°C -13.7 and -29.7 kJ were obtained for both reactions.

TABLE IV The Gibbs Energy of Reactions

	Reaction	$-\log P_{O_2}$ (atm)	-ΔG° (kJ)	-Δ <i>G</i> <sup>∞</sup> (kJ)
(1) Pr <sub>4</sub> Co <sub>3</sub> O	$\frac{1}{10} + \frac{1}{4}O_2 = \frac{1}{2}Pr_2O_3 + 3PrCoO_3$	$2.05 \pm 0.03$	$15.8 \pm 0.2$	13.7
(2) $Pr_4Co_3O_1$	$_{10} + CoO + \frac{1}{2}O_2 = 4PrCoO_3$	$3.05 \pm 0.03$	$41.7 \pm 0.8$	29.7
(3) 3Pr <sub>2</sub> CoO	$4 + \frac{1}{2}O_2 = Pr_4Co_3O_{10} + Pr_2O_3$	$3.10 \pm 0.03$	$58.4 \pm 0.5$	
(4) 2Pr <sub>2</sub> CoO	$_{4} + CoO + \frac{1}{2}O_{2} = Pr_{4}Co_{3}O_{10}$	$3.60 \pm 0.03$	$57.3 \pm 0.6$	
(5) $PT_2O_3 +$	$CoO + 0.04O_2 = Pr_2CoO_{4.08}$	$5.73 \pm 0.06$	$6.1 \pm 0.1$	
(6) $\frac{1}{2}$ Sm <sub>2</sub> O <sub>1</sub>	$+$ CoO $+$ $1O_2 =$ SmCoO <sub>1</sub>	$1.82 \pm 0.05$	$12.4 \pm 0.5$	
$(7) \frac{1}{2}Eu_2O_3 +$	$+$ CoO + $\frac{1}{2}O_2 = EuCoO_3$	$1.42 \pm 0.03$	9.6 ± 0.5	
(8) <sup>1</sup> / <sub>2</sub> Tb <sub>2</sub> O <sub>3</sub> +	$-CoO + \frac{1}{2}O_2 = TbCoO_3$	$0.53 \pm 0.07$	$3.3 \pm 0.5$	

<sup>a</sup> Cherepanov et al. (8).



FIG. 5. The relationship between the ionic radius of lanthanoid elements in 12 coordination and  $\Delta G^{\circ}$  values of reaction,  $\frac{1}{2}Ln_2O_3 + CoO + \frac{1}{4}O_2 = LnCoO_3$ .

The latter value is higher than the present value, but the reason for the difference is not yet clear.

# (3) The Relationship between $\Delta G^{\circ}$ and Ionic Radius

In the previous report (2), the Gibbs energy of the reaction,  $\frac{1}{2}Ln_2O_3 + CoO + \frac{1}{4}O_2 = LnCoO_3$ , showed a linear change with the ionic radius of lanthanoid elements with 12 coordination. It is of interest whether or not the present three values fit on the previous linear line. In Fig. 5 these values were plotted with open circles together with the previous three. They fit well. The values for LaCoO<sub>3</sub> and PrCoO<sub>3</sub> fit especially well despite the difference of the crystal system

from other perovskite structures. This implies that the crystal system has a smaller effect on  $\Delta G^{\circ}$  than the ionic radius.

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